

Optimization and Control in Shell Models of Turbulence

Forcing optimization of the GOY model

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Content

- 1 Context
 - Fluid Mechanics
 - Navier-Stokes equations
- 2 Main body of work & study
 - Shell Models
 - GOY Model
 - Parameter space & energy
 - Process and complex variable separation
 - Linearization of the equations
- 3 Numerical Integration and Optimization
 - Understanding the Optimization Problem
 - Runge-Kutta methods
- 4 Conclusions and further work
- 5 Bibliography

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Fluid Mechanics

- Conservation of Mass
- Conservation of Momentum
- Energy equation

Turbulence and Laminar Flow

- What is Turbulence and Laminar Flow
- Reynolds number
 - $Re = \frac{\rho u L}{\mu}$
- Main characteristics

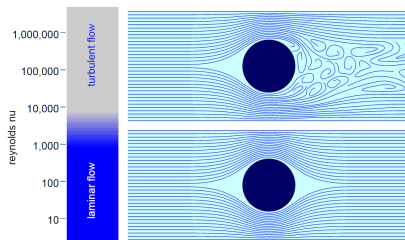


Figure:

Examples of turbulent and fluid dynamics

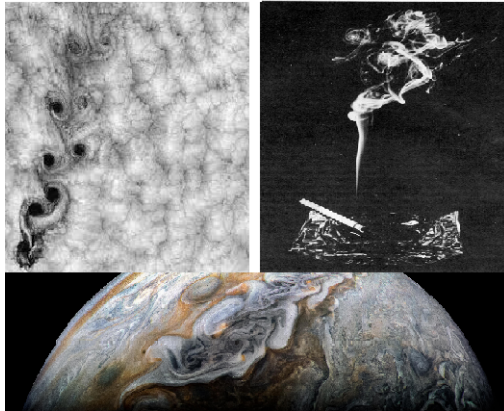


Figure: Atmospheric flow over Selkirk Island; Laminar to Turbulent flow in cigarette smoke; Jupiter turbulent gases

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Navier-Stokes equations

History and context

- Contributions made by Claude Navier & George Stokes
- Use and examples of Navier-Stokes equations
- Complexity and possible solutions

The equations

- Continuity Equation
- Momentum Equations

Three Dimensional components:

$$\nabla \cdot \vec{V} = 0$$

$$\rho \frac{D\vec{V}}{Dt} = -\nabla p + \rho \vec{g} + \mu \nabla^2 \vec{V}$$

+ boundary conditions + inicial conditions

Shell Models & Energy

- Structure
- Reasoning behind Shell Models

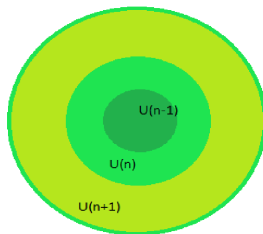


Figure:

Shell Models & NSE

- Kolmogorov 1941 energy spectrum
- Invariants preserved to mimic the Navier-Stokes equations
- Energy cascade spectrum & energy transfer in shell models

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Turbulence in Shell Models & NVE

- Fluid Mechanics and Turbulence basics
- Energy Density and Spectral energy Flux
- The four-fifth law
- Parameter Space for the GOY model
- 2D and 3D models

Kolmogorov Theory

Velocity in the K41

The state of the flow is characterized by the mean energy dissipation per unit mass: $\bar{\epsilon}$

Velocity difference: $\delta u(l) \equiv |u(r+l) - u(r)|$, eddy of size $l \ll L$;

$\delta u(l) = f(\tilde{l}, \bar{\epsilon})$ by dimensional analysis:

$$[\delta u] = m s^{-1}; [l] = m; [\bar{\epsilon}] = m^2 s^{-3}$$

$$[\delta u] = [l]^\alpha [\bar{\epsilon}]^\beta \implies \alpha = \beta = 1/3$$

$$\text{Resulting in: } \lambda \delta u(l) = f[\lambda(\bar{\epsilon} l)^{1/3}]$$

Kolmogorov Theory

Scale and Dissipation

With the previous result and the NSE we can estimate the rate of change of the energy per unit volume due to dissipation at scale η , when it becomes important in contrast to L .

$$\bar{\epsilon} \sim \nu u_i \partial_{jj} u_i \sim \nu \delta u(\eta)^2 / \eta^2$$

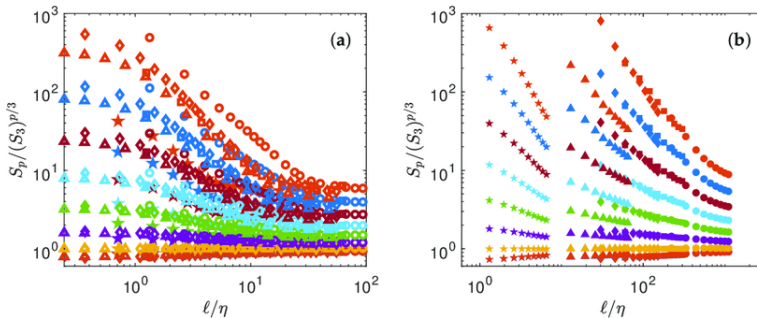
So the Kolmogorov scale:

$$\eta \sim (\bar{\epsilon} / \eta^3)^{-1/4} \text{ depends on the Reynolds numbers as } \eta \sim Re^{-3/4}$$

Numeric simulation

The energy cascade can be visualized by setting different base parameters.

Figure:



Spectral energy density

- The mean of the square of the velocity difference is called second order structure function:
- $S_2(l) \equiv \langle \delta u(l)^2 \rangle \sim (\bar{\epsilon}l)^{2/3}$ is related to the spectral energy density through a Fourier transform.
- We can also express the energy density of the flux:
 - $E = \frac{1}{2} \int u(x)^2 dx = \frac{1}{2} (2\pi)^3 \int_0^\infty u_i(k) u_i(k)^* dk = \frac{1}{2} (2\pi)^3 4\pi \int_0^\infty k^2 |u(k)|^2 dk \equiv \int_0^\infty E(k) dk$
- Using the Parseval's identity in fourier transforms of spectral velocities:
 - $\frac{1}{(2\pi)^3} \int u_i(x) u_i(x) dx = \int u_i(-k') u_i(k') dk' = \int u_i(k') u_i(k')^* dk'$ with $u_i(x) \in \mathbb{R} \implies u_i(-k') = u_i(k')^*$

Spectral energy density

- Integration was performed over the sphere and absorbing the spacial variable into dx , results in:
 - $E(k) = (2\pi)^4 k^2 |u(k)|^2$ and $S_2(l) = \int [u(l+x) - u(x)]^2 dx$
 - Combining both equations and after several complex integration processes we obtain:
 - $E(k) = \frac{1}{2\pi k} \int_0^\infty x \sin(x) S_2(x/k) dx \sim \bar{\epsilon}^{-2/3} k^{-5/3}$

Spectral energy density

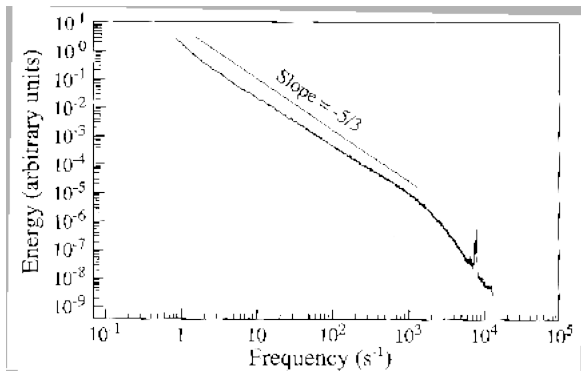


Figure:

The four-fifth law

- A special case occurs for a third order structure function, associated with energy conservation. Again considering a homogeneous and isotropic turbulent fluid left alone after intense stirring. As the kinetic change is 0, the mean energy dissipation is:

- $\bar{\varepsilon} = -\frac{1}{2}\partial_t [u]$

Scaling relation

After several integrations and calculation regarding isotropy and the NSE, remains a simple equation regarding the third order structure function:

$$S_3 = -\frac{4}{5}\bar{\epsilon}l$$

This law is a cornerstone of fluid dynamics. Not only is it in agreement with the phenomenology described in the K41 as it is exact and among few exact results derived from NSE.

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GOY Model

- Gledzer & Obukhov

Model and given inicial conditions

- $\mathcal{L}u = f_n$

- $\mathcal{L}u =$

$$\frac{du_n}{dt} - ik_n \left(u_{n+1}u_{n+2} - \frac{\varepsilon}{q}u_{n+1}u_{n-1} + \frac{\varepsilon-1}{q}u_{n-2}u_{n-1} \right)^* + \nu k_n^2 u_n$$

- Constants used
- Force and solution for the GOY model

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Parameter Space for the GOY model

- Number of Shells
- Kinematic viscosity
- Initial force
- Free Parameters

Values used

$$N = 24; \nu = 10^{-7}; f_n = (1 + i) \times 5 \times 10^{-3}$$

2D and 3D models

- 2D/3D selector
- Complex non linear coefficients

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Constant manipulation and restraints

- Constants changed

GOY model constant substituiton

- $a_n = k_n = k_0 q^n$
- $b_n = -\frac{1}{2}k_{n-1}$
- $c_n = -\frac{1}{2}k_{n-2}$

- All components with shell index, $n \leq 0$ are taken as zero
- Resulting in:

$$\left(\frac{d}{dt} + vk_n^2\right) u_n = i(a_n u_{n+1} u_{n+2} + b_n u_{n+1} u_{n-1} + c_n u_{n-1} u_{n-2})^* + f_n$$

Separation

- Splitting complex variables $u_n = x_n + iy_n$:

Real Part

$$\left(\frac{d}{dt} + vk_n^2\right) x_n = a_n (x_{n+1}y_{n+2} + x_{n+2}y_{n+1}) + b_n (x_{n-1}y_{n+1} + x_{n+1}y_{n-1}) + c_n (x_{n-2}y_{n-1} + x_{n-1}y_{n-2}) + f_x$$

Imaginary Part

$$\left(\frac{d}{dt} + vk_n^2\right) y_n = ia_n (x_{n+1}x_{n+2} - y_{n+2}y_{n+1}) + ib_n (x_{n-1}x_{n+1} - y_{n+1}y_{n-1}) + ic_n (x_{n-2}x_{n-1} - y_{n-1}y_{n-2}) + if_y$$

Verification

- Jupyter Notebook, Python, algorithm used to verify the separated variables equations.

Algorithm

- Load a complex variable with pseudo-random numbers ($u = x + iy$);
- Write the complex GOY model in simple for loops, all the $N=24$ shells;
- Write the separated GOY equations as for loops;
- Write a function that retrieves the difference between the 3 functions;
- Return the biggest difference (0 meaning these equations were well determined).

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Process

Linearized the system of real and imaginary equations around set solutions.

Simple example

$$\begin{bmatrix} x_n \\ y_n \end{bmatrix} = \begin{bmatrix} \tilde{x}_n \\ \tilde{y}_n \end{bmatrix} + \varepsilon \begin{bmatrix} x_n \\ y_n \end{bmatrix}$$

The term of order ε^2 will not be considered ($\varepsilon \ll 1$)

Linear Scheme

$$\frac{d}{dt} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ \vdots \\ x_n \\ y_1 \\ y_2 \\ y_3 \\ \vdots \\ y_n \end{bmatrix} = -\nu \begin{bmatrix} k_1^2 x_1 \\ k_2^2 x_2 \\ k_3^2 x_3 \\ \vdots \\ k_n^2 x_n \\ k_1^2 y_1 \\ k_2^2 y_2 \\ k_3^2 y_3 \\ \vdots \\ k_n^2 y_n \end{bmatrix} + \begin{bmatrix} C_1 & C_2 \\ C_3 & C_4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ \vdots \\ x_n \\ y_1 \\ y_2 \\ y_3 \\ \vdots \\ y_n \end{bmatrix} + ,$$

where the block matrices C_1, C_2, C_3, C_4 , are given by:

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Adjoint operator

- Cost functional in the separated variables equations
- Determining the adjoint operator and transpose matrix

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Classic fourth order RK

Generic expression

$$u^{n+1} = u^n + \Delta t \sum b_i k_i$$

Initial Value Problem

$$y' = f(t, y); y(t_0) = y_0$$

$$y_{n+1} = y_n + \frac{h}{6}(k_1 + 2k_2 + 2k_3 + k_4)$$

$$t_{n+1} = t_n + h$$

Classic fourth order RK & GOY model

RK4

$$k_1 = f(t_n, y_n)$$

$$k_2 = f\left(t_n + \frac{h}{2}, y_n + \frac{h}{2}k_1\right)$$

$$k_3 = f\left(t_n + \frac{h}{2}, y_n + \frac{h}{2}k_2\right)$$

$$k_4 = f(t_n + h, y_n + hk_3)$$

$$h = 10^{-4}; n \approx 2.5 \times 10^8$$

Computing the problem and force optimization

Optimization Process

- Choosing an initial guess $f^{(0)}$; $n = 0$
- Solve the GOY model equations, with $f = f^{(0)}$
- Solve the adjoint operator from matrix C1...
- Obtain the cost functional gradient
- Find a parameter...
- Update the variable and repeat.

Finding the particular solution

Process

$$\left(\frac{d}{dt} + vk_n^2\right) u_n = i(a_n u_{n+1} u_{n+2} + b_n u_{n+1} u_{n-1} + c_n u_{n-1} u_{n-2})^* + f_n$$

- A solution is calculated for every time step.
- A solution consists of 24 pairs of real and imaginary numbers.

Finding other solutions and changing the initial force.

Plugging the solutions $x_n y_n$ and using the Runge Kutta method for integration, we find solutions for the values \widetilde{x}_n & \widetilde{y}_n .
Python algorithm was used to find these solutions.

Algorithm

Using the GOY separated equations $x_n; y_n$ are found for a certain δt . Using RK4

Using the linearized equations, and matrices C1, C2, C3, C4 for each time step:

\widetilde{x}_n and \widetilde{y}_n are calculated

Repeat the process

Expected iterations around 2×10^8

Conclusions

The force optimization process and the verification of convergence for the solutions was not fully completed, mostly due to lack of time, but also to some limitations in Python.

It would have been better to do the long computing algorithms in a simpler language such as Fortran. The objective of the long numeric runs was to find the optimal force or approaching it, optimal in a way that would recreate and verify the energy cascade found in the GOY model and in the K41.

Context

Main body of work & study

Numerical Integration and Optimization

Conclusions and further work

Bibliography

Bibliography and References



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